Dobkin

| [54] | INPUT SUPPLY INDEPENDENT CIRCUIT     |  |
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| [51] | Int. Cl. <sup>2</sup><br>Field of Se | 307/297; 323/4; 330/199<br>                                |
| [56] |                                      | References Cited   |

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**UNITED STATES PATENTS** 

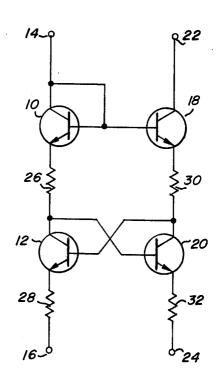
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#### **ABSTRACT**

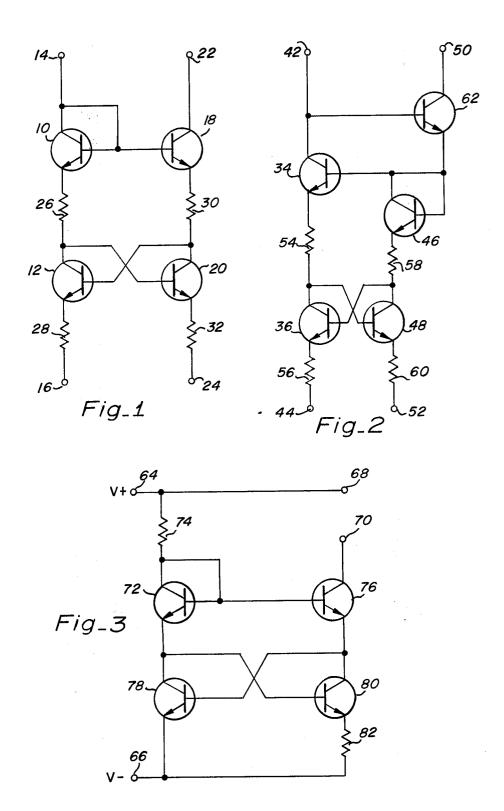
A circuit includes a plurality of transistors which are biased by a supply to provide an output which is independent of that supply and dependent only on the

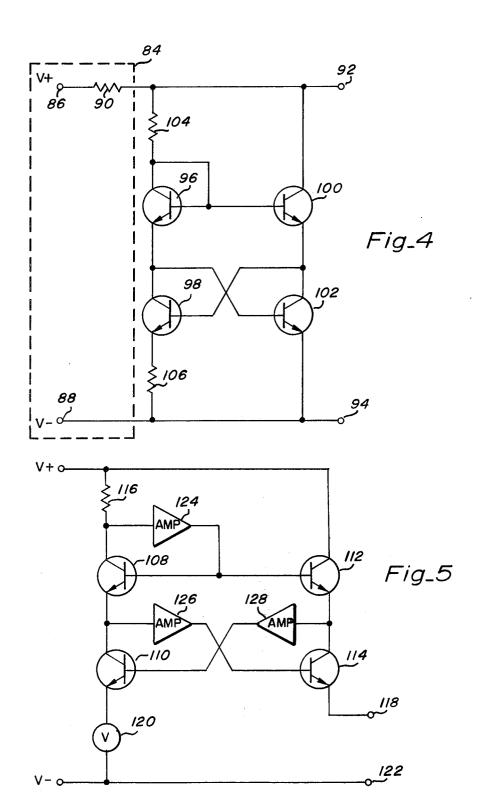
summation of the base-emitter voltages of the transistors, if any. A first pair of transistors are connected in series with one another between the supply and a second pair of transistors are connected in series with one another between the supply. The base-emitter junctions of the transistors are connected in a series loop, such that a voltage is developed between the baseemitter junctions of two adjacent transistors which is equal to the base-emitter voltage summation. The base-emitter voltages of any series connected transistors oppose one another in the series loop. Since the collector currents of the series connected transistors are equal to one another and their base-emitter voltages oppose one another in the series loop, the baseemitter voltage summation will be independent of collector currents and, therefore, independent of the input supply. The circuit can be employed as either a voltage or current regulator. As a regulator circuit, the emitter area of one transistor is different than the emitter area of another transistor, such that the summation of the base-emitter voltages will be other than zero and independent of the input supply. The circuit can also be employed as a buffer amplifier by making the emitter areas of the transistors equal to one an-

### 16 Claims, 5 Drawing Figures









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# INPUT SUPPLY INDEPENDENT CIRCUIT

#### **BACKGROUND OF THE INVENTION**

#### 1. Field of the Invention

This invention relates generally to a circuit having an output which is independent of its input supply, and more particularly to such a circuit in which a voltage related to the output voltage thereof is developed which is proportional only to the difference of the emitter areas of transistors.

#### 2. Prior Art

Various types of circuits require an output which is independent of the input voltage or current supply. It has been the usual practice in the past to isolate the output of such circuits from the input supply with a relatively large number of components. This practice has resulted in relatively large and complex circuits. Since the cost of an integrated circuit is related to the number of components contained therein and to the complexity thereof, it is desirable to reduce the number of components required to produce a particular result to a minimum. Furthermore, the operation of such circuits is subject to processing parameters, rather than solely to basic transistor parameters, and such processing parameters are not easily controlled.

A good example of a circuit which requires its output to be independent of its input supply is a regulator circuit. A high degree of current or voltage regulation 30 in integrated circuits has required relatively complex circuits in the past. For example, a Zener diode voltage regulator requires several stages of current amplification to reduce the dynamic impedance of the circuit to provide a well regulated voltage supply output. A relatively large number of components is required to provide the desired amount of current amplification and to decrease the dynamic impedance sufficiently to provide such a regulated supply.

Another type of circuit which requires its output to be independent of its input supply is a buffer amplifier. In a buffer amplifier, such as a voltage follower or current amplifier, it is desirable to have the voltage of the input signal source reflected exactly at the output, with a relatively high impedance input and low impedance output. If the output of such an amplifier is not independent of its input supply, variations in that supply will affect the output and the input voltage will not be reflected exactly at such output. Furthermore, if such output is dependent upon processing parameters, rather than solely on basic transistor parameters, the output cannot be well defined.

Accordingly, it can be appreciated that a need exists for a circuit which will provide an output which is independent of its voltage or current supply without being relatively complex, requiring a large number of components, and which is independent of processing parameters. More particularly, a need exists for such a circuit which is formed of relatively few components and is 60 dependent only on basic transistor parameters for its operation, which parameters are capable of being controlled within relatively close tolerances.

# SUMMARY OF THE INVENTION

Accordingly, it is a primary object of the present invention to provide a circuit having an output which is independent of its voltage or current supply.

Another object of the present invention is to provide a circuit having an output which is independent of its supply and has relatively few components.

A further object of the present invention is to provide such a circuit in which its operation is independent of processing parameters and dependent only on basic transistor parameters.

Still another object of the present invention is to provide a regulator circuit which requires relatively few components and which has a relatively high degree of regulation.

Yet another object of the present invention is to provide either a voltage or current regulator having an output which is unaffected by changes in its supply voltage or current.

A further object of the present invention is to provide such a voltage or current regulator which requires relatively few components to perform its function.

Another object of the present invention is to provide a buffer amplifier in which the voltage of an input signal source is reflected exactly at an output thereof.

Still another object of the present invention is to provide such a buffer amplifier having a relatively high impedance input and a relatively low impedance output.

A further object of the present invention is to provide such a buffer amplifier in which a relatively high current output can be provided without a current limiting resistor.

These and other objects of the present invention are attained by a transistor circuit in which an output voltage is developed which is equal to the summation of the base-emitter voltages of the transistors. This output voltage is employed to provide either a well regulated voltage or current output, or to reflect an input voltage exactly at an output of the circuit.

A feature of the present invention resides in maintaining the collector currents of any transistors connected in series equal to one another and their base-emitter voltages around a series loop opposing one another, such that the summation of the base-emitter voltages of the transistors is proportional only to the difference in emitter areas of the transistors, if any. If such a difference exists, the output voltage will be proportional thereto and other than zero. However, if such a difference does not exist, the output voltage will be zero and an input signal source can be reflected exactly at an output of the circuit.

Another feature of the present invention resides in the provision of a resistor in any one of the emitter circuits of the transistors, such that various output characteristics can be obtained.

The invention, however, as well as other objects, features and advantages thereof will be more fully realized and understood from the following detailed description, when taken in conjunction with the accompanying drawings, wherein:

# BRIEF DESCRIPTION OF THE DRAWINGS

- FIG. 1 is a circuit diagram of a four terminal network constructed in accordance with the principles of the present invention.
- FIG. 2 is a circuit diagram of an alternate embodiment of the four terminal network of the present invention.
  - FIG. 3 is a circuit diagram of a current regulator constructed in accordance with the principles of the present invention.

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FIG. 4 is a circuit diagram of a voltage regulator constructed in accordance with the principles of the present invention.

FIG. 5 is a circuit diagram of a buffer amplifier constructed in accordance with the principles of the present invention.

# DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

With reference to FIG. 1, there is shown a four terminal network which is constructed in accordance with the principles of the present invention. A pair of transistors 10 and 12 have their collector-emitter circuits connected in series with one another between a pair of terminals 14 and 16. A pair of transistors 18 and 20 have their collector-emitter circuits connected in series with one another between a pair of terminals 22 and 24. Resistors 26, 28, 30 and 32 are connected in the emitter circuits of the transistors 10, 12, 18 and 20, respectively. The value of any one or all of the resistors 26–32 may be zero. Preferrably, only one of the resistors 26–32 will have a value other than zero.

It can be appreciated from FIG. 1 that the base-emitter junctions of the transistors 10, 12, 18 and 20 are connected serially in a loop with one another. That is, beginning with the terminal 16, the loop includes the resistor 28, the base-emitter junction of the transistor 12, the resistor 30, the base-emitter junction of the transistor 18, the base-emitter junction of the transistor 10, the resistor 26, the base-emitter junction of the transistor 20, and the resistor 32. If the terminal 16 is connected to the terminal 24 and only one of the resistors 26-32 has a value other than zero, the summation of the base-emitter voltages of the transistors will be developed on that resistor.

In the above described serial loop, the base-emitter voltage of the transistor 12 opposses the base-emitter voltage of the transistor 10 and the base-emitter voltage of the transistor 20. Also, the base-emitter voltage of the transistor 20 opposes the base-emitter voltage of the transistor 18. Since the transistors 10 and 12 have their collector-emitter circuits connected in series, their collector currents will be equal. It can be appreciated that the collector currents of the transistors 18 and 20 will also be equal. Accordingly, the summation of the base-emitter voltages of all of the transistors will be proportional to the difference of their emitter areas. That is, the difference of the base-emitter voltages,  $\Delta V_{be}$ , which is the voltage developed across one of the resistors 26-32 having a value other than zero, is defined by the expression:

$$\Delta V_{bc} = \frac{KT}{q} \ln \frac{J_{c2}}{J_{c1}} \tag{1}$$

where  $J_{c_1}$  is the combined current density of the transistors 12 and 18 and  $J_{c_2}$  is the combined current density of the transistors 10 and 20. Accordingly, if the emitter areas of the transistors are of different values, the current density ratio of the above expression will be other than zero. It can be appreciated, therefore, that the voltage of an input source which supplies a bias to each of the transistors 10, 12, 18 and 20 will not affect the summation of the base-emitter voltages,  $\Delta V_{be}$ , developed on one of the resistors 26–32 which has a value other than zero. It can also be appreciated that this summation of the base-emitter voltages,  $\Delta V_{be}$ , will be

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zero if all of the emitter areas of the transistors are equal to one another.

An alternate embodiment of a four terminal network constructed in accordance with the principles of the present invention is illustrated in FIG. 2. As shown therein, transistors 34 and 36 are connected in series between a pair of terminals 42 and 44 and transistors 46 and 48 are connected in series between a pair of terminals 50 and 52. Resistors 54, 56, 58 and 60 are connected in the emitter circuits of the transistors 34, 36, 46 and 48, respectively. It can be appreciated from the drawings and the above description that the circuit thus described in FIG. 2 is similar to the circuit illustrated in FIG. 1. A transistor 62 has its collector-emitter circuit connected in series between the terminal 50 and the collector of the transistor 46 and has its base connected to the terminal 42. The transistor 62 isolates the collector of the transistor 46 from any voltage changes which may occur on the terminal 50 and raises the output impedance of the circuit.

With reference to FIG. 3, there is shown a current regulator which is constructed in accordance with the principles of the present invention. A voltage source, represented by V+ and V-, is connected to terminals 64 and 66. The circuit of FIG. 3 is operative to provide a constant current through a load (not shown) when it is connected across terminals 68 and 70, regardless of variations in the supply voltage on the terminals 64 and 66.

The collector of a transistor 72 is connected through a resistor 74 to the terminal 64 and 68, to its base, and to the base of a transistor 76 having its collector connected to the terminal 70. The collector-emitter circuit of the transistor 72 is connected in series with the collector-emitter circuit of a transistor 78 and the collector-emitter circuit of a transistor 76 is connected in series with the collector-emitter circuit of a transistor 76 is connected in series with the collector-emitter circuit of a transistor 80. The junction between the transistors 72 and 78 is connected to the base of the transistor 80 and the junction between the transistors 76 and 80 is connected to the base of the transistor 78. The emitter of the transistor 78 is connected to the terminal 66 and the emitter of the transistor 80 is connected through a resistor 82 to the terminal 66.

The current regulator illustrated in FIG. 3 is one example of a practical embodiment of the circuit illustrated in FIG. 1. The only constraint on the circuit illustrated in FIG. 3 is that the resistor 74 must be of a value to provide a current therethrough which is greater than the output current of the transistor 72 divided by its beta. From inspection of the circuit, it will be appreciated that the voltage developed across the resistor 82 is equal to the sum of the base-emitter voltages of the transistors 76 and 78 less the sum of the 55 base-emitter voltages of the transistors 72 and 80. Since the summation of the base-emitter voltages of the transistors 72-80 is proportional to the difference of their emitter areas, if any, the voltage developed on the resistor 82 will also be proportional to that summation. For example, if the emitter areas of the transistors 72 and 78 are equal and, since their collector currents are equal, their base-emitter voltages will cancel one another. In such an example, the voltage developed across the resistor 82 will equal to the base-emitter voltage of the transistor 76 less the base-emitter voltage of the transistor 80. This difference of the base-emitter voltages is defined by the above expression where J<sub>c</sub> and J<sub>c</sub> are current densities of the transistors 76 and 80,

respectively. It can be appreciated that the load current, which is equal to the current through the resistor 82, will remain constant since its value depends upon the ratio of the current densities of the transistors and such ratio will, of course, remain constant, since the collector currents of the transistors having their collector-emitter circuits in series are equal to one another.

With reference to FIG. 4, there is shown a voltage regulator circuit which employs the principles of the circuit illustrated in FIG. 1. A current source, represented diagrammatically by a dotted outline block which is designated with the reference numeral 84, includes a voltage source designated by V+ and V-connected to terminals 86 and 88 and a resistor 90. It is to be understood, of course, that any current source may be employed for supplying the circuit. The circuit of FIG. 4 supplies a regulated voltage across a pair of terminals 92 and 94.

Transistors 96, 98, 100 and 102 are connected in the same configuration as that of FIG. 1. The collector of the transistor 96 is connected through a resistor 104 to one side of the supply 84 and to the terminal 92. The emitter of the transistor 98 is connected through a resistor 106 to the terminals 88 and 94.

The voltage developed across the resistor 106 is equal to the sum of the base-emitter voltages of the transistors 96 and 102 less the sum of the base-emitter voltages of the transistors 98 and 100. Since the voltage developed across the resistor 106 is independent of its resistance value, a low regulated voltage is developed thereon. This regulated voltage is reflected at the terminals 92 and 94 as an output voltage having a high degree of regulation. Furthermore, this voltage will be proportional to the difference of the emitter areas of the transistors and will be independent of the current supply 84 and the voltage supply on the terminals 86 and 88.

The circuit illustrated in FIG. 4 performs such voltage regulation by controlling the current through the transistors 100 and 102 to maintain the voltage on the terminals 92 and 94 constant. The value of the voltage developed on the terminals 92 and 94 is determined by the difference of the emitter areas of the transistors. From inspection, it can be appreciated that the voltage across the terminals 92 and 94,  $V_s$ , is defined by the expression:

$$V_s = \Delta V_{br} \frac{R_2}{R_1} + V_{br1} + V_{br2}, \qquad (2)$$

where  $\Delta V_{be}$  is the difference of the base-emitter voltages of the transistors having different emitter areas,  $R_2$  is the value of the resistor 104,  $R_1$  is the value of the resistor 106,  $V_{be_1}$  is the base-emitter voltage of the transistor 96, and  $V_{be_2}$  is the base-emitter voltage of the transistor 102. Since the first quantity in the above expression (2) has a positive temperature coefficient and the two remaining quantities have a negative temperature coefficient, at a particular output voltage on the terminals 92 and 94, the circuit will exhibit a zero temperature coefficient. More particularly, such a zero temperature coefficient occurs when the output voltage on the terminals 92 and 94 is equal to 2.4 volts or 2 times the extrapolated band gap of silicon.

When the supply current attempts to increase, the conduction level of the transistors 100 and 102 will increase, to shunt current therethrough so that the

voltage on the resistor 106 remains constant. By maintaining the voltage on the resistor 106 constant, the voltage across the terminals 92 and 94 will also remain constant.

The circuit illustrated in FIG. 5 is a buffer amplifier which employs the principles of the circuit illustrated in FIG. 1. It can be appreciated from the drawing that the transistors 108, 110, 112 and 114 are connected together to form the circuit illustrated in FIG. 1 when all of the resistors 26–32 have a value of zero. One side of a voltage supply, designated V+, is connected to the collector of the transistor 112 and through a resistor 116 to the collector of the transistor 108. The emitter of the transistor 114 is connected to one output terminal 118 and the emitter of the transistor 110 is connected through an input signal source 120 to the other side of the voltage supply, designated V-, and to another output terminal 122.

If the emitter areas of the transistors 108-114 are equal to one another, the voltage of the input signal source 120 will be reflected exactly on the terminals 118 and 122. It can be appreciated that the input signal source 120 can be any source, including the circuit illustrated in FIG. 4. The circuit of FIG. 5 presents a relatively high impedance to the input signal source 120 and provides a relatively low impedance output on the terminals 118 and 122. Furthermore, a relatively high current output can be provided across the terminals 118 and 122 without a current limiting resistor in the circuit.

Since the limit of the circuit illustrated in FIG. 5 is controlled by the betas of the transistors 108–114, the base drive to each of those transistors can be increased to permit a relatively high output current across the terminals 118 and 122. More particularly, a current amplifier 124 supplies a base drive to each of the transistors 108 and 112, a current amplifier 126 supplies a base drive to the transistor 114, and a current amplifier 128 supplies a base drive to the transistor 110. Accordingly, the base drive for all of the transistors is not derived from the voltage source designated V+ and V-, but is derived from the amplifiers 124, 126, and 128. Since the voltage gain of each of the amplifiers 124, 126 and 128 is unity, the voltage developed across the terminals 118 and 122 will not be affected thereby.

It can be appreciated that the circuit illustrated in FIG. 2 can also be employed as a current regulator, a voltage regulator and a buffer amplifier, Furthermore, the circuits illustrated in FIGS. 1 and 2 can be employed to provide a variety of input and output characteristics by controlling the values of the resistors 26-32 and the resistors 54-60.

The Invention claimed is:

1. A circuit disposed for connection to an input supply for providing an output which is independent of that supply, comprising

a plurality of transistors, and

means responsive to the input supply for generating a base-emitter voltage on all of said transistors,

the base-emitter junctions of said transistors being connected serially in a loop with one another, such that the summation of the base-emitter voltages of said transistors is developed as an output voltage between the base-emitter junctions of two adjacent ones of said transistors in said loop,

the collector currents of any of said transistors having their collector-emitter circuits connected in series being equal to one another and their base-emitter

voltages opposing one another around said loop, such that said summation of the base-emitter voltages is independent of the collector currents of said transistors and only proportional to the difference of the emitter areas of said transistors.

- 2. The circuit of claim 1, wherein the emitter areas of at least two of said transistors are different from one
- 3. The circuit of claim 2, wherein said output voltage 10 is proportional to the difference of the emitter areas of said transistors.
- 4. The circuit of claim 3, further comprising a resistor connected between the base-emitter junctions of said two adjacent transistors, such that said output voltage 15 is developed on said resistor, and wherein the current through said resistor is available at the collector of one of said transistors as an output.
- 5. The circuit of claim 3, further comprising a resistor connected between the base-emitter junctions of said two adjacent transistors, such that said output voltage is developed on said resistor, and wherein the current through one of said transistors is proportional to the value of said resistor.
- 6. The circuit of claim 1, wherein said plurality of transistors includes a first pair of transistors having their collector-emitter circuits connected in series and a second pair of transistors having their collector-emitter circuits connected in series, and wherein said gener- 30 ating means includes a first connection from the junction between said first pair of transistors to the base of a first one of said second pair of transistors, a second connection from the junction between said second pair of transistors to the base of a first one of said first pair of transistors, and a third connection between the base of a second one of said first pair of transistors to the base of a second one of said second pair of transistors.
- 7. The circuit of claim 6, wherein said generating means further includes a fourth connection from the collector of one of said second transistors to its base.

8. The circuit of claim 7, wherein said generating means further includes a plurality of current amplifiers, one in each of said first, second and third connections.

9. The circuit of claim 8, wherein the collectors of said second transistors are disposed for connection to one side of the input supply and the emitter of one of said first transistors is disposed for connection through an input voltage source to the other side of the input supply.

10. A four terminal network, comprising a. a first pair of transistors having their collector-emitter circuits connected in series between a first pair of terminals,

- b. a second pair of transistors having their collectoremitter circuits connected in series between a second pair of terminals,
- c. a connection from one of the first pair of terminals to the base of a first one of said first pair of transistors and to the base of a first one of said second pair of transistors,

d. a connection from the junction of said first pair of transistors to the base of a second one of said second pair of transistors, and

e. a connection from the junction of said second pair of transistors to the base of a second one of said first pair of transistors.

11. The network of claim 10, further comprising a resistor connected in the emitter circuit of one of said transistors.

12. The network of claim 11, wherein said resistor is connected between said first pair of transistors.

13. The network of claim 11, wherein said resistor is connected between said second pair of transistors.

- 14. The network of claim 11, wherein said resistor is connected between the emitter of said second one of said first pair of transistors to a second one of the first 35 pair of terminals.
  - 15. The network of claim 11, wherein said resistor is connected between the emitter of said second one of said second pair of transistors to one of the second pair of terminals.
  - 16. The network of claim 10, further comprising an amplifier in each of said connections.

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